

Recent Developments in RheoSANS

Katie Weigandt (NIST)

June 7th 2017

canSAS Workshop

Acknowledgements

Steve Hudson (NIST)
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Daniel Blair (Georgetown U)

Lionel Porcar (ILL)
Joao Cabral (Imperial College London)

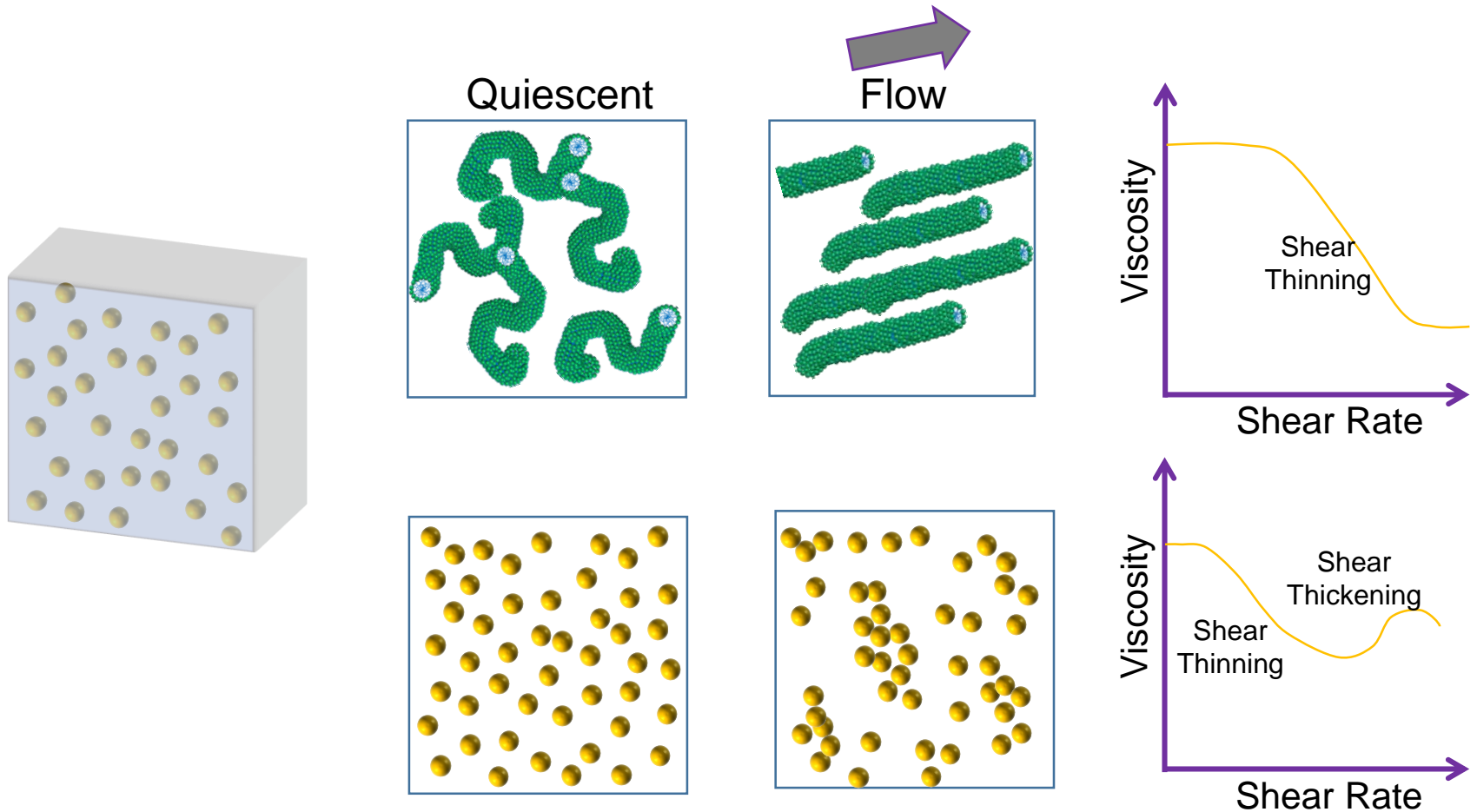
Matt Helgeson (UC Santa Barbara)
Nino Ruocco (UC Santa Barbara)
Patrick Corona (UC Santa Barbara)

Carlos Lopez-Barron (Exxon-Mobile)
Jeff Richards (NIST)

Lynn Walker (Carnegie Mellon)
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RheoSANS -- Introduction



Current Opinion in Colloid & Interface Science 17 (2012) 33–43

Flow-SANS and Rheo-SANS applied to soft matter

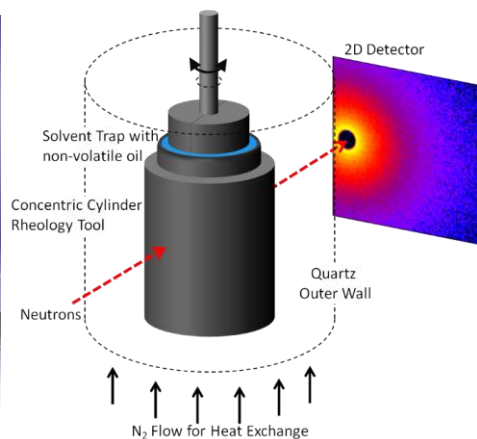
Aaron P.R. Eberle ^a, Lionel Porcar ^{b,*}

^a NIST Center for Neutron Research, National Institute of Standards and Technology, Gaithersburg, MD, 20899, USA

^b Large Scale Structure Group, Institut Laue Langevin, Grenoble, France

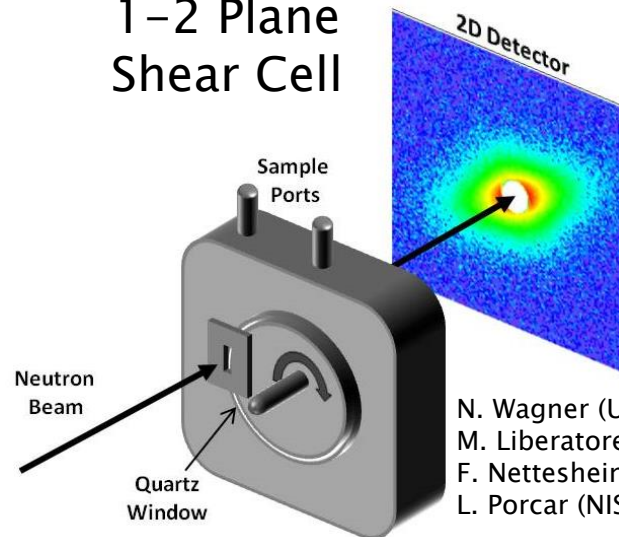
RheoSANS-Status quo

RheoSANS



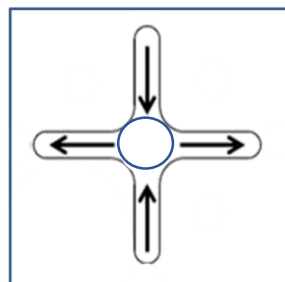
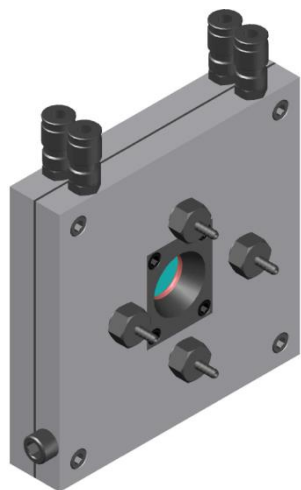
L. Porcar (NIST), J. Moyer (NIST), P. D. Butler (NIST), L. D. Pozzo (NIST, UW)
G. Langenbacher (Anton Paar)

1-2 Plane Shear Cell

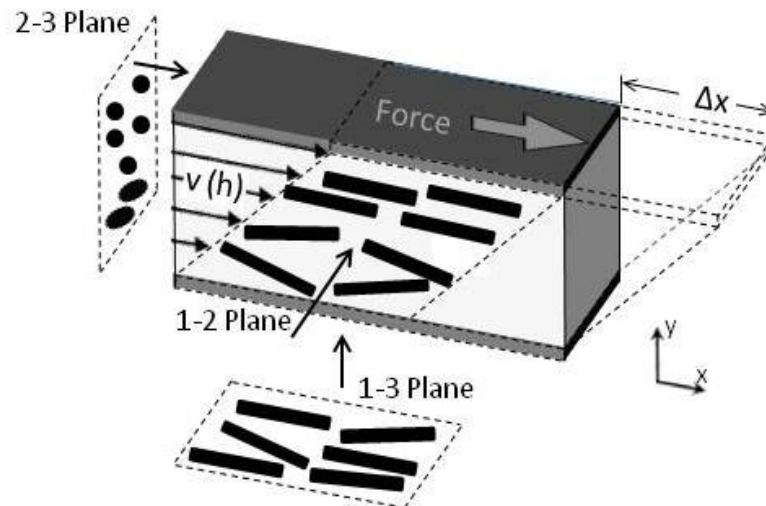


N. Wagner (UDeI)
M. Liberatore (UDeI)
F. Nettesheim (UDeI)
L. Porcar (NIST)

Extensional Flow Cell



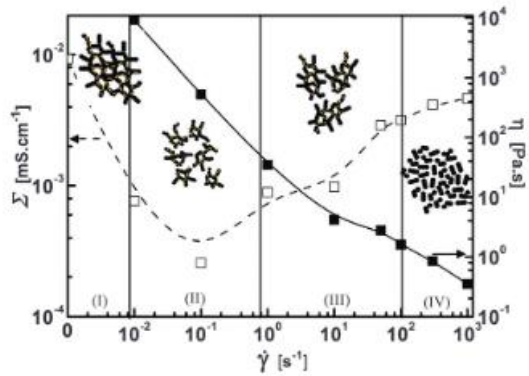
K. Weigandt (NIST)
Koty McAllister (UDEI)



Measure Simultaneous Rheology, Structure and...

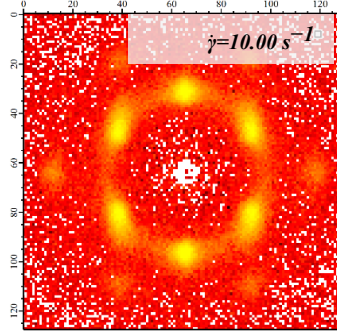
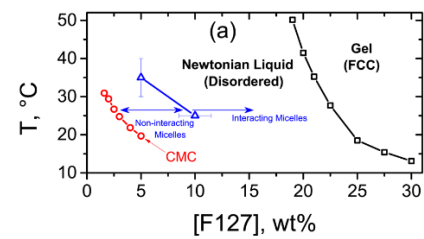
Dielectric RheoSANS: Motivation

Carbon Black Suspensions for Flow Battery Electrodes



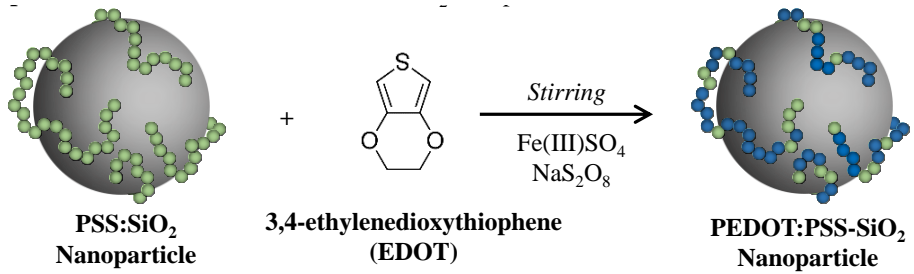
Youssrey et al. Chem. Phys (2013) 15, 14476

Ion Conduction through Self-Assembled Porous Materials Ordered by Flow



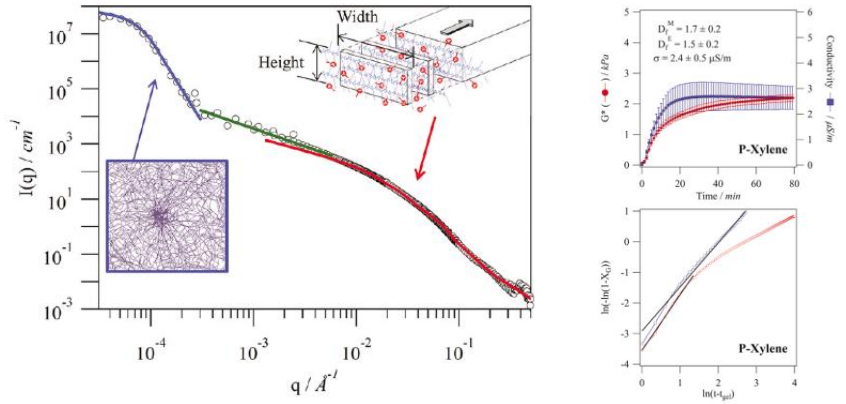
Lopez-Barron et al. Macromolecules (2014) 47.7484

Next Generation Conductive Additives



Richards et al. ACS Applied Materials and Interfaces (2016)

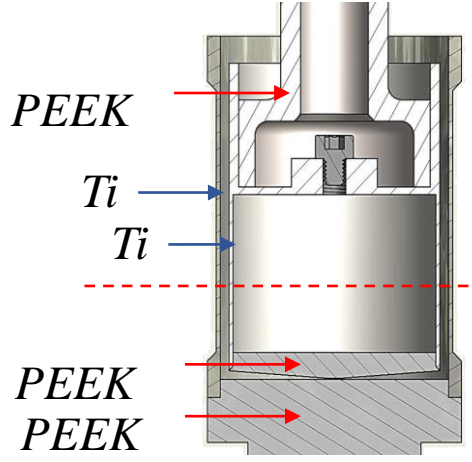
Self-Assembled Semiconducting Nanofibers



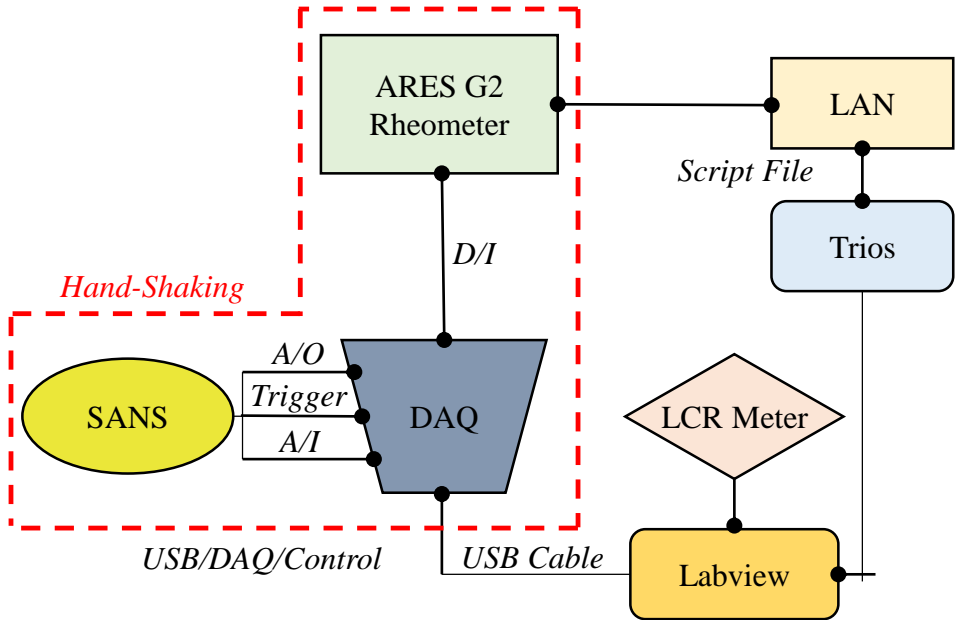
Newbloom et al. Macromolecules (2012) 45.3452-3462

Dielectric RheoSANS: Experiment

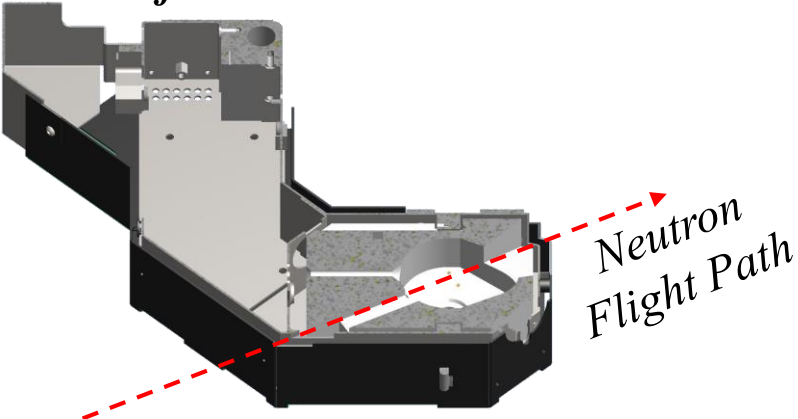
Dielectric RheoSANS Geometry



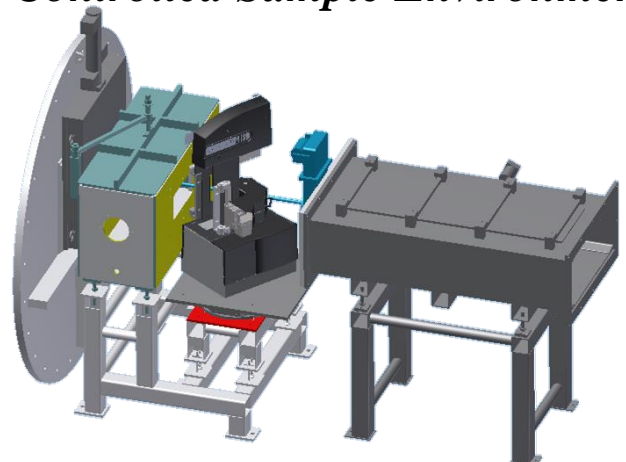
ARES G2 Synchronization Protocol



Modified Oven Cross-Section



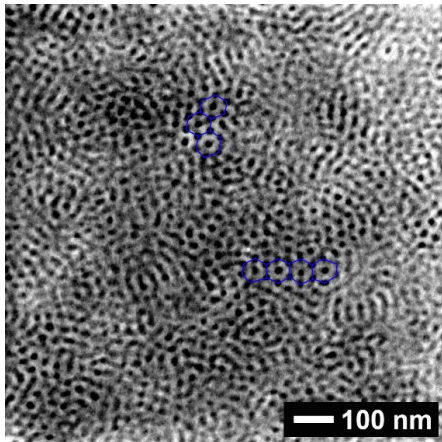
Strain-Controlled Sample Environment



Other Rheometer Options (Extensional Strain)

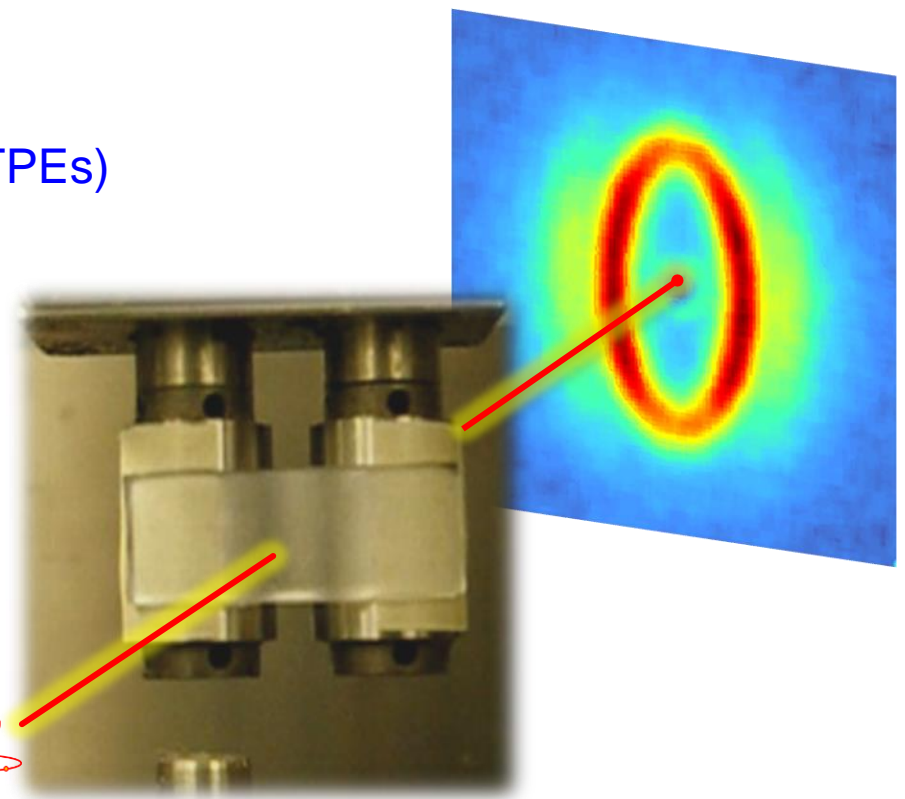
Extensional Strain

Example 1: Thermoplastic Elastomers (TPEs)



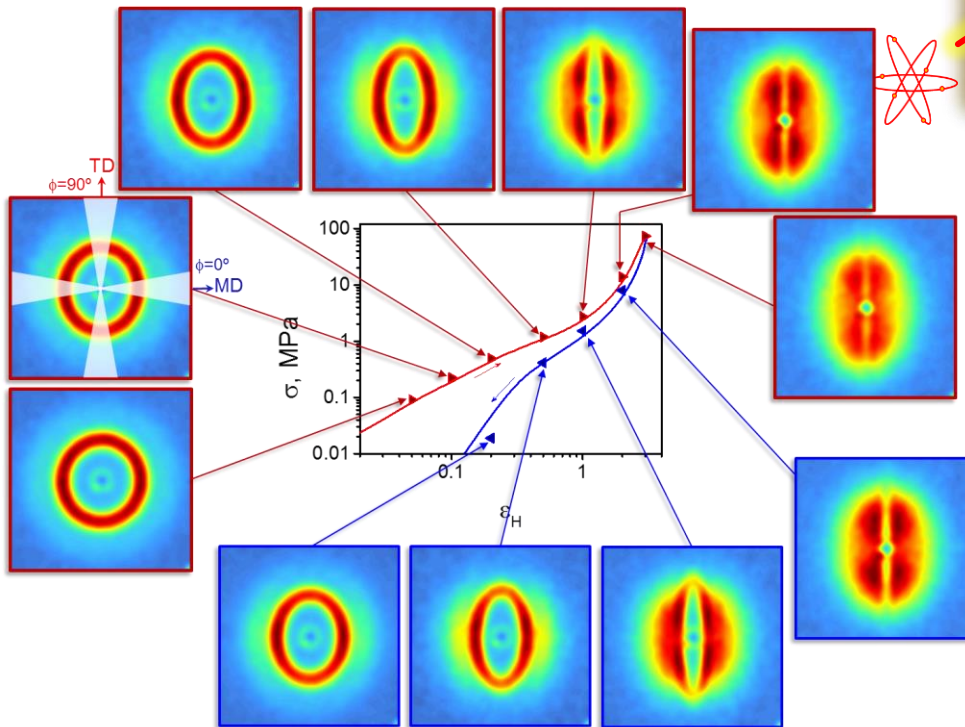
TPE:
SIS triblock copolymer

Stretched at
room temperature



Sentmanat Extensional
rheometer (SER):

Ideal geometry for
in-situ scattering
measurements

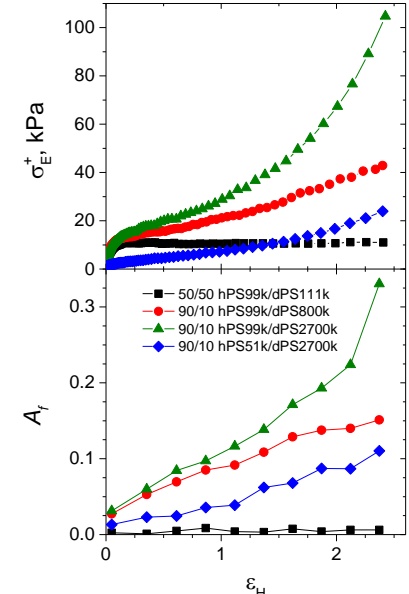
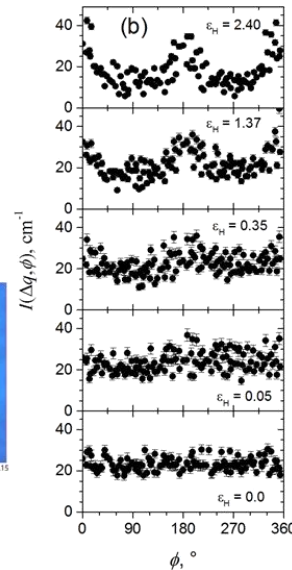
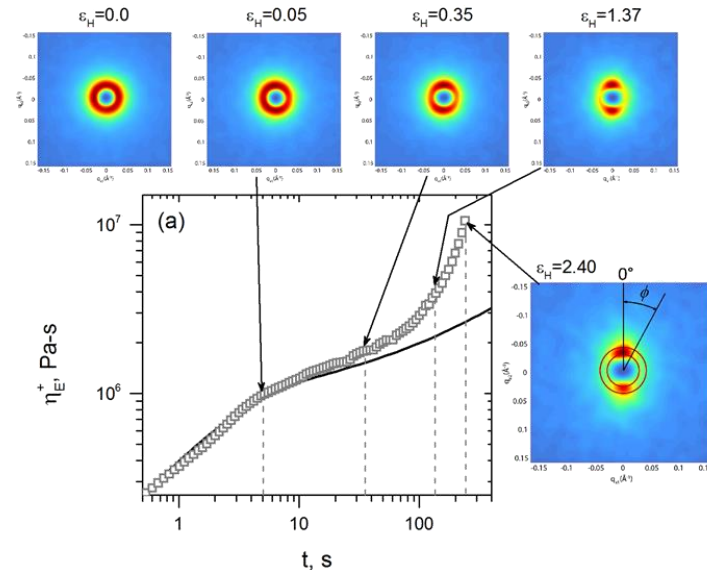
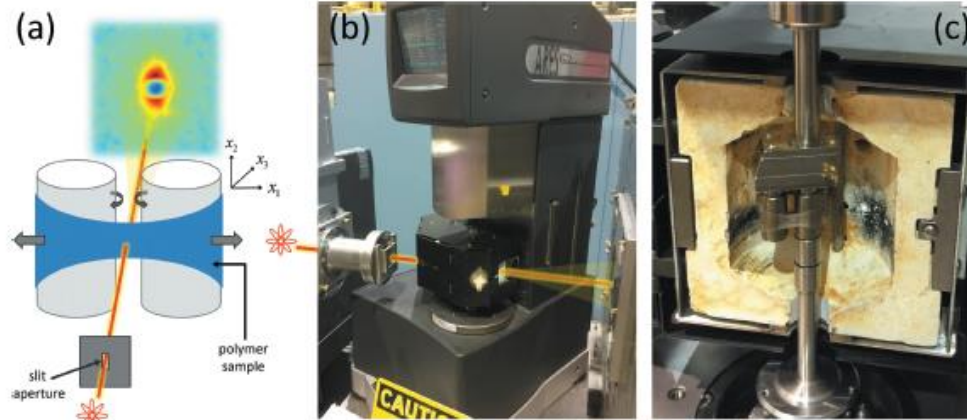


López-Barrón et al., *Rheol. Acta* **55**, 103 (2016)

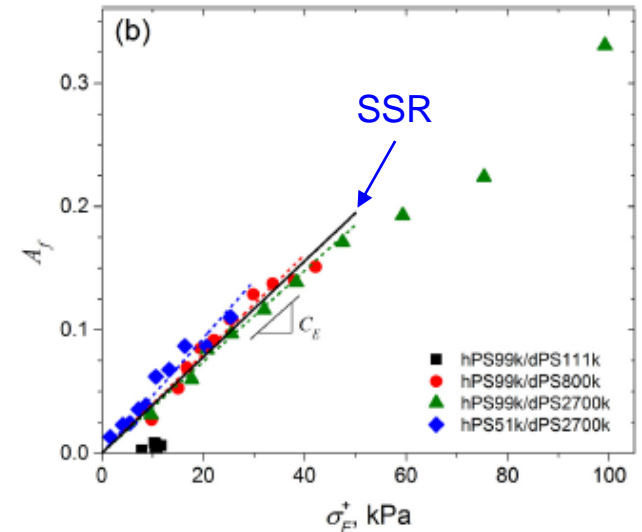
Extensional Strain

Example 3: Polymer melts

Sample: Polystyrene (H/D Isotope blends)
 Stretched in the melt (at 150 °C) using time-resolved SANS

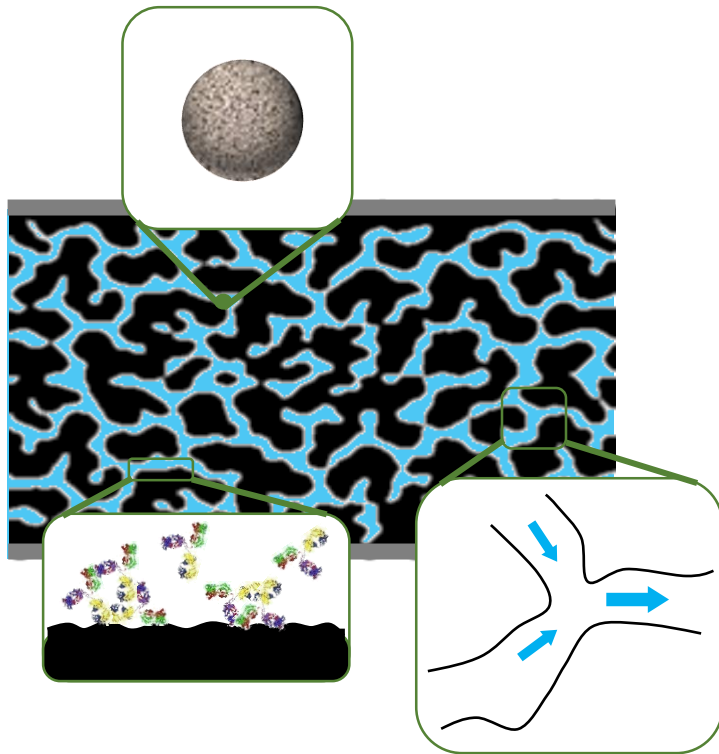


Stress-SANS rule (analogous to stress-optic rule):

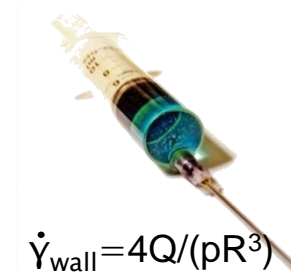


Realistic and Industrially Relevant Flow Conditions

It is often very difficult to measure the nanostructure of complex fluids in dynamic and industrially relevant environments!



High Strain/Flow Rates
($\sim 1,000,000 \text{ s}^{-1}$)



$$\dot{\gamma}_{\text{wall}} = 4Q/(\pi R^3)$$

Non-Ambient Conditions

High Temperatures
($> 200^\circ\text{C}$)

High Pressures
(up to 70 MPa)



and

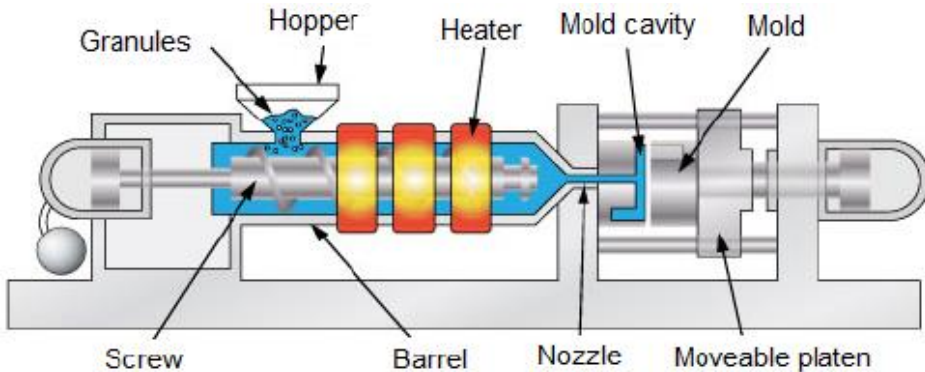


Toward *real* processing flows

Real processing flows involve a range of deformation types and histories.

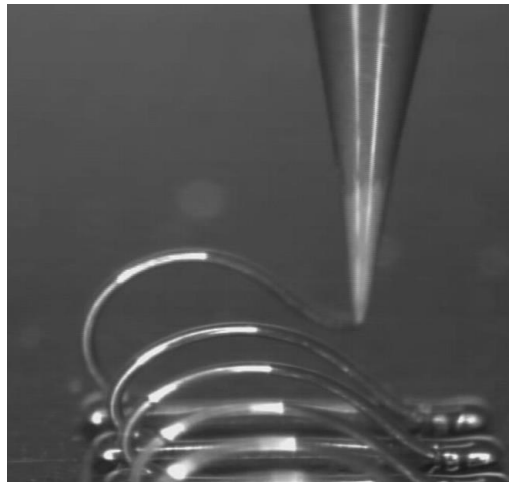
Injection molding

R. Svečko et al., Sensors, 2013, 13(5).



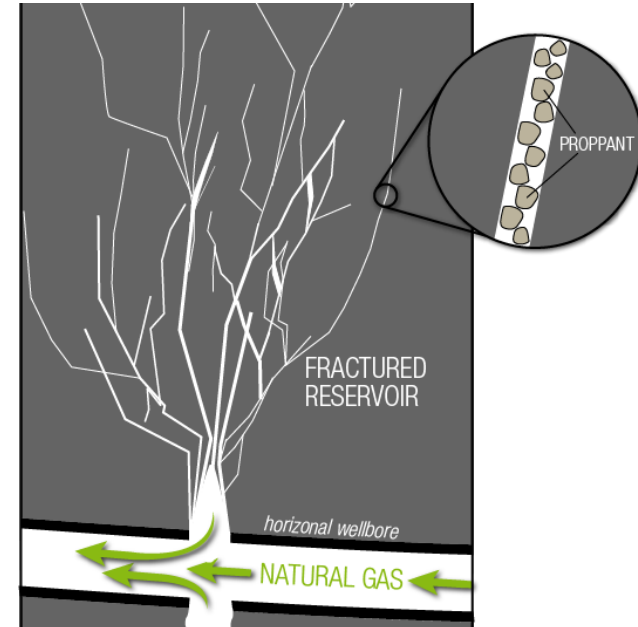
3D printing

B.Y. Ahn et al., Science, 2009, 323(5921).



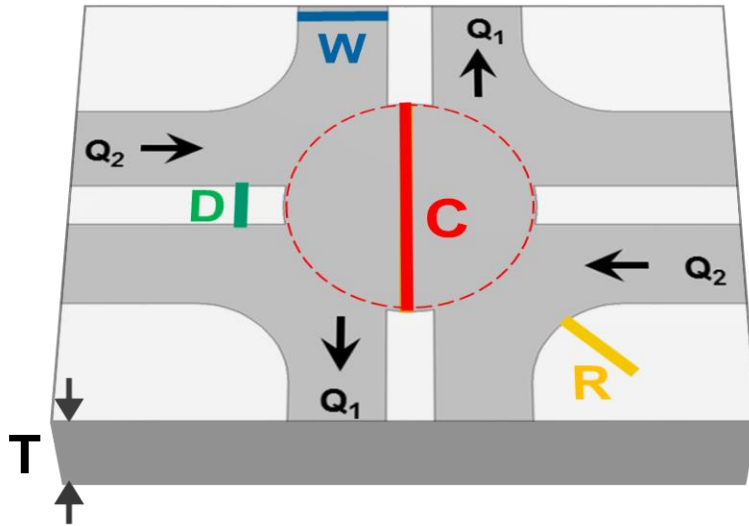
Hydraulic fracturing

Indiana Geological Survey



A fluidic four-roll mill (FFoRM) for arbitrary deformations

Fluidic four-roll mill (FFoRM)



Straining in an arbitrary 2D flow

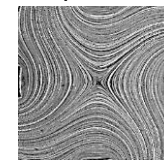
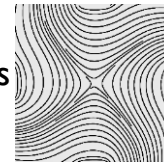
$$\dot{\Gamma} = \frac{1}{2}(\nabla \underline{u} + \nabla \underline{u}^T)^{1/2} = \frac{\dot{\Gamma}}{2} \begin{bmatrix} \Lambda & 1 - \Lambda \\ 1 - \Lambda & \Lambda \end{bmatrix}$$

Flow type parameter: $\Lambda = \Lambda(Q_2/Q_1)$
 Rate of strain: $\dot{\Gamma} = \dot{\Gamma}(Q_1)$

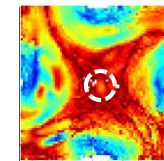
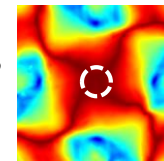
Extension ($\Lambda = 1$)

Simulation

Experiment



Streamlines

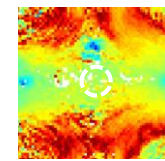
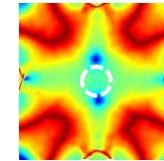
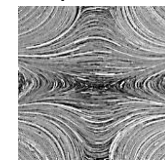
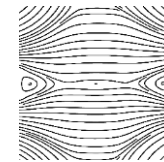


Flow type, Λ

Shearing ($\Lambda = 0$)

Simulation

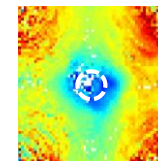
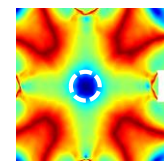
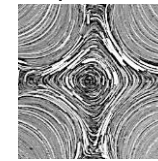
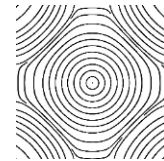
Experiment



Rotation ($\Lambda = -1$)

Simulation

Experiment



Λ

1.0

0.5

0.0

-0.5

-1.0

Advantages over other designs:

- Uniform, Lagrangian-steady deformation type/rate
- Long residence time in beam area (steady state)
- Λ and $\dot{\Gamma}$ can be arbitrarily varied

in time

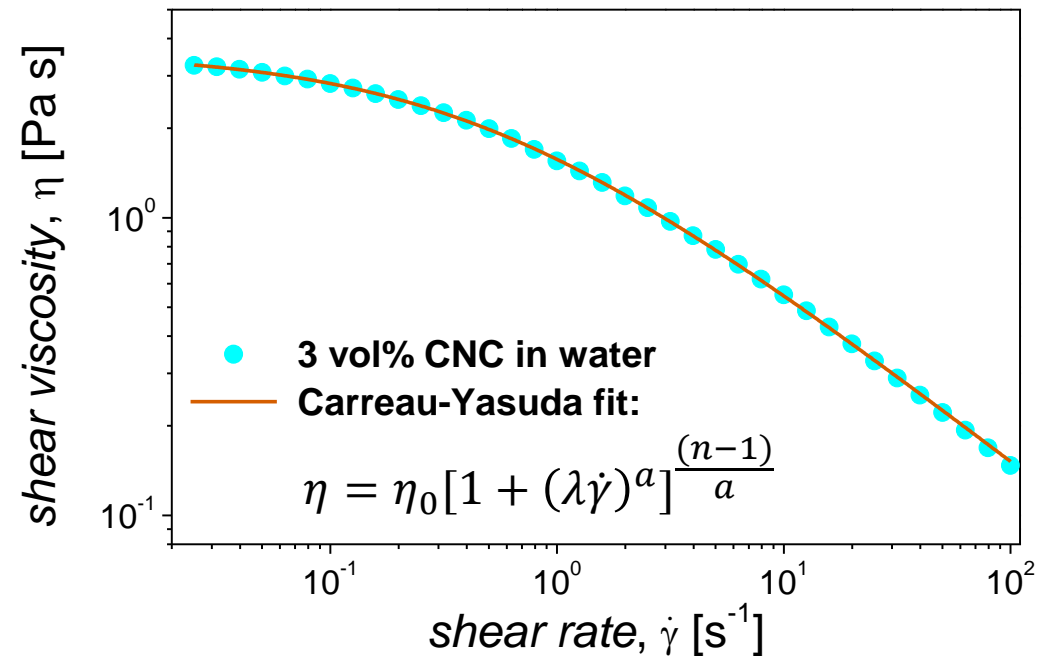
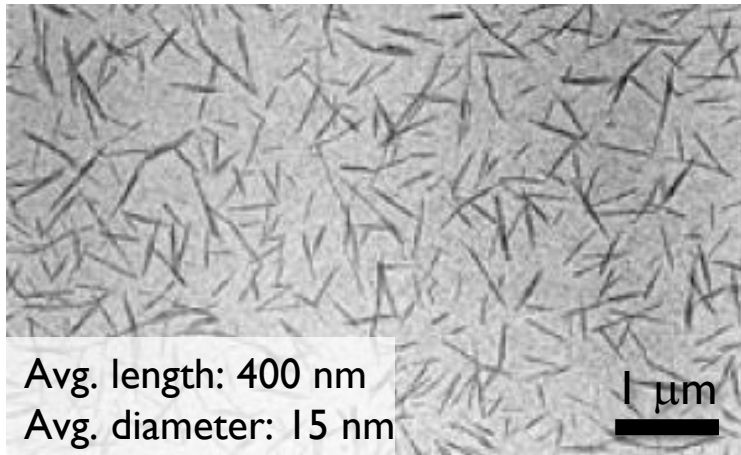
UC SANTA BARBARA
 chemical
 engineering

Helgeson group, UCSB, *in preparation.*

(white circles are 1 mm)

Model test fluid – colloidal rod suspensions

Cellulose nanocrystals
(3.3 vol% in D₂O)



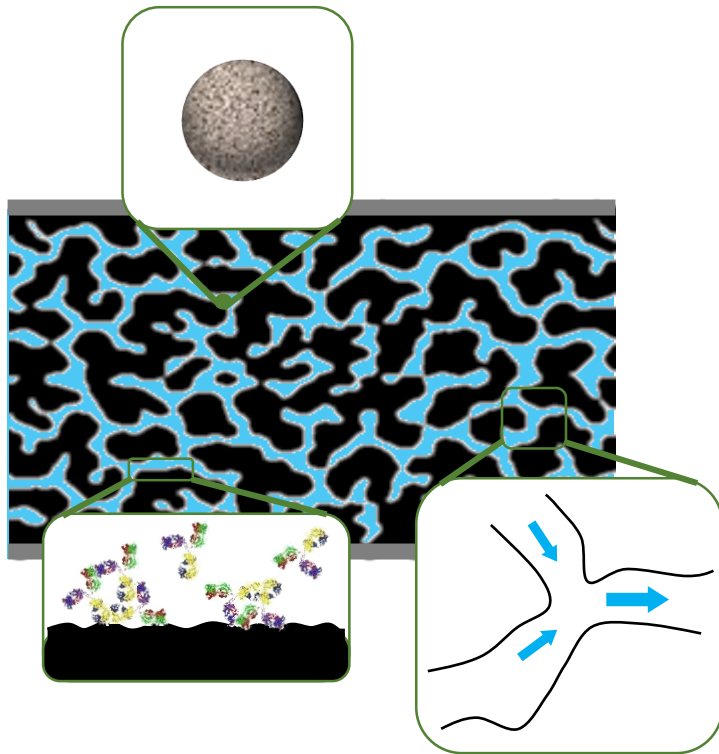
Exact microscopic theory for dilute colloidal rod suspensions¹

Dilute rods in 2D flow:

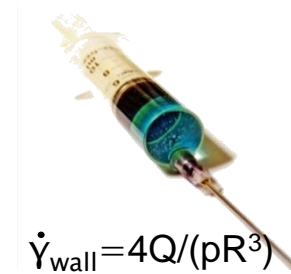
$$\theta_0(\Lambda) = \arccos \left(\sqrt{\frac{1}{2} + \frac{\sqrt{\Lambda}}{1+\Lambda}} \right)$$

[1] Bird, Armstrong, Hassager and Curtiss, Dynamics of Polymeric Liquids, Wiley, 1977.

It is often very difficult to measure the nanostructure of complex fluids in dynamic and industrially relevant environments!



High Strain/Flow Rates
($\sim 1,000,000 \text{ s}^{-1}$)



$$\dot{\gamma}_{\text{wall}} = 4Q/(\pi R^3)$$

Non-Ambient Conditions

High Temperatures
($> 200^\circ\text{C}$)

High Pressures
(up to 70 MPa)

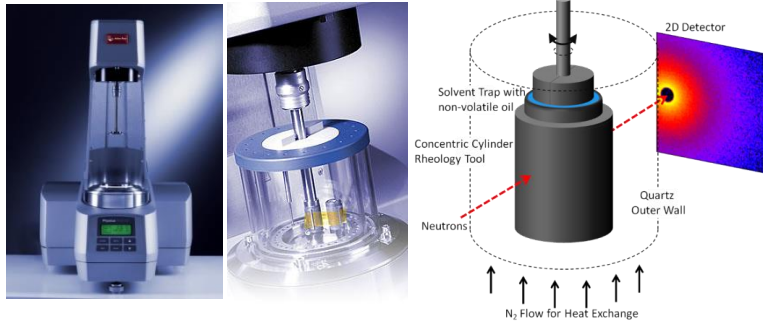


and



μ RheoSANS -- Requirements

RheoSANS



L. Porcar (NIST), J. Moyer (NIST), P. D. Butler (NIST), L. D. Pozzo (NIST, UW)
G. Langenbacher (Anton Paar)

Desired Capabilities

Temperature **>200°C**

Pressure **up to 70 MPa**

Shear Rate **up to 10⁶ s⁻¹**

RheoSANS Capabilities

Temperature **-50°C to 200°C**

Pressure **Atmospheric**

High Shear Rate + Low Shear Stress

Shear Rate **12,000 s⁻¹**

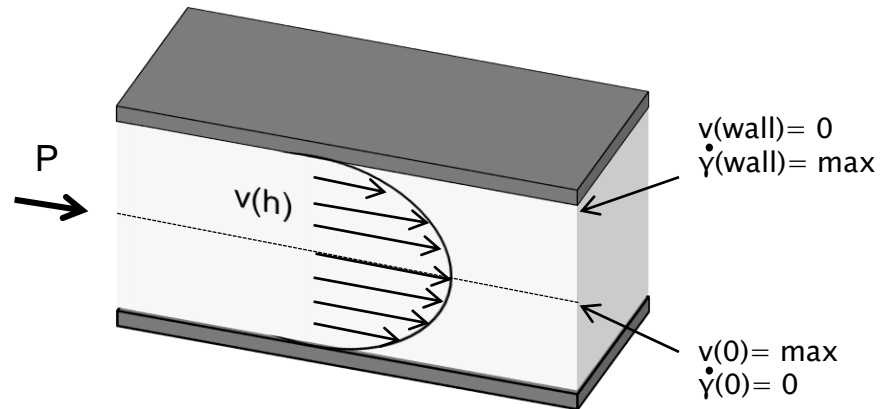
Shear Stress **900 Pa**

Low Shear Rate + High Shear Stress

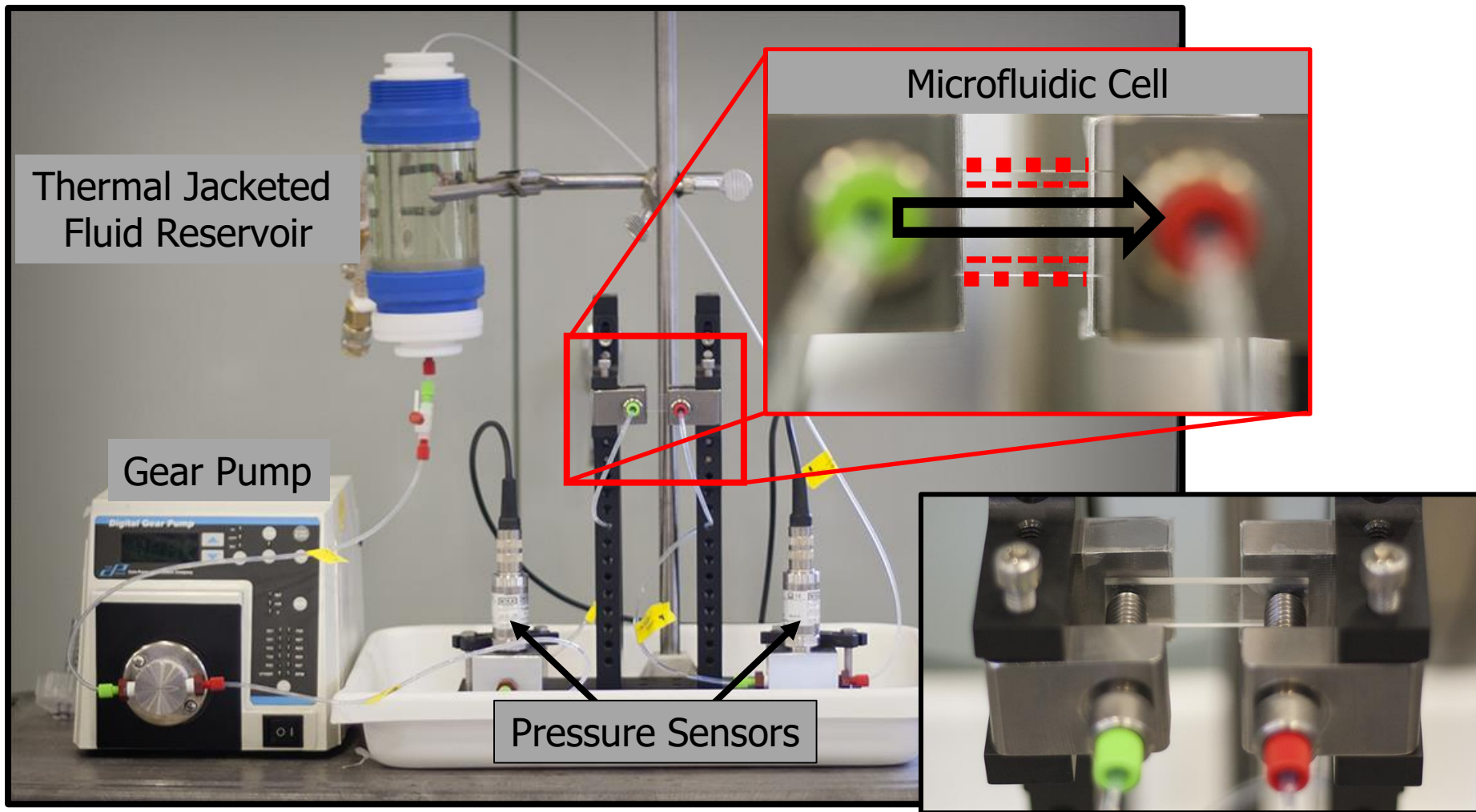
Shear Rate **3,500 s⁻¹**

Shear Stress **4,500 Pa**

Pressure Driven Flow/Capillary Rheometry



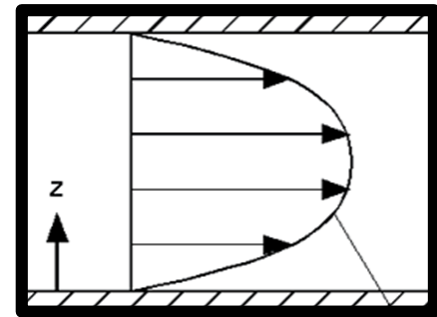
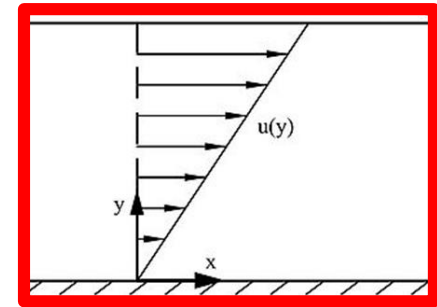
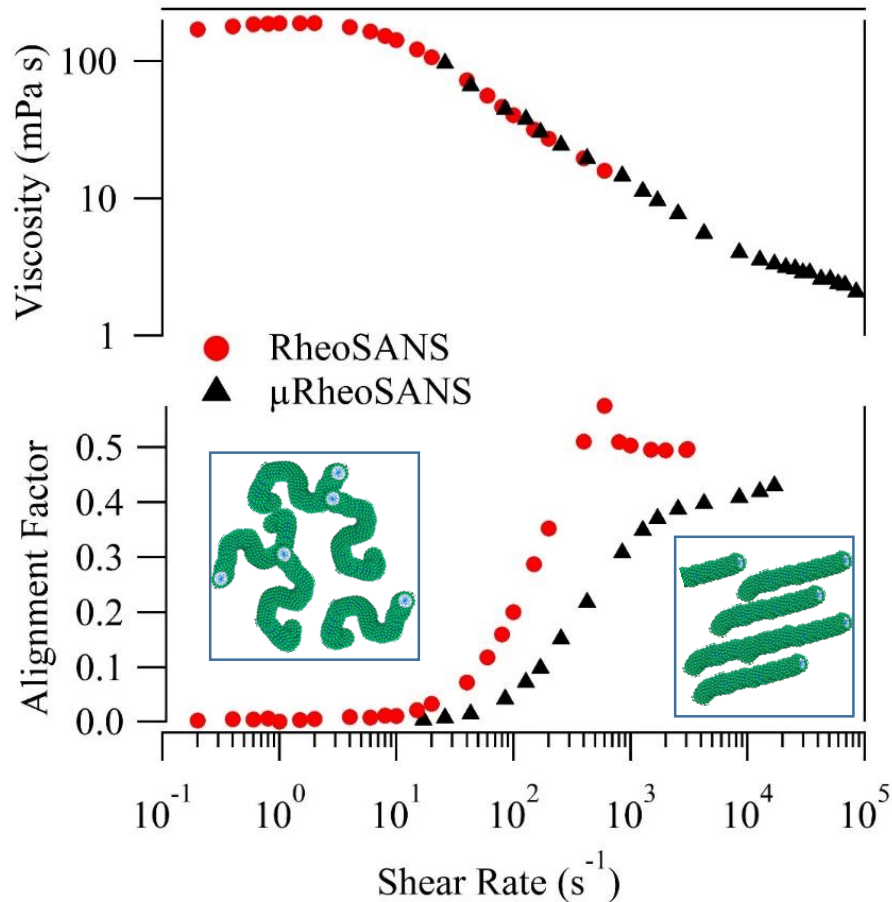
μ RheoSANS -- Prototype



Weston, Seeman, Salipante, Blair, Hudson and Weigandt (In Preparation)

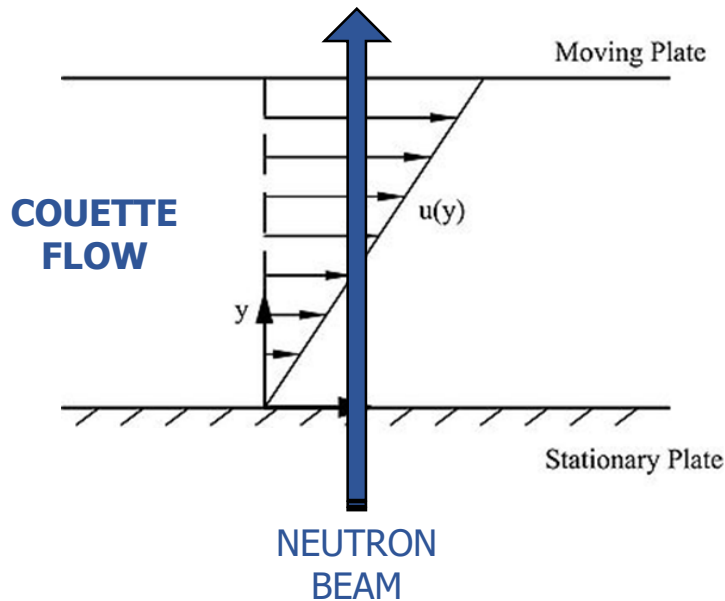
μ RheoSANS of Anionic Wormlike Micelles

1.15% Steol CS460/8% NaCl in D₂O

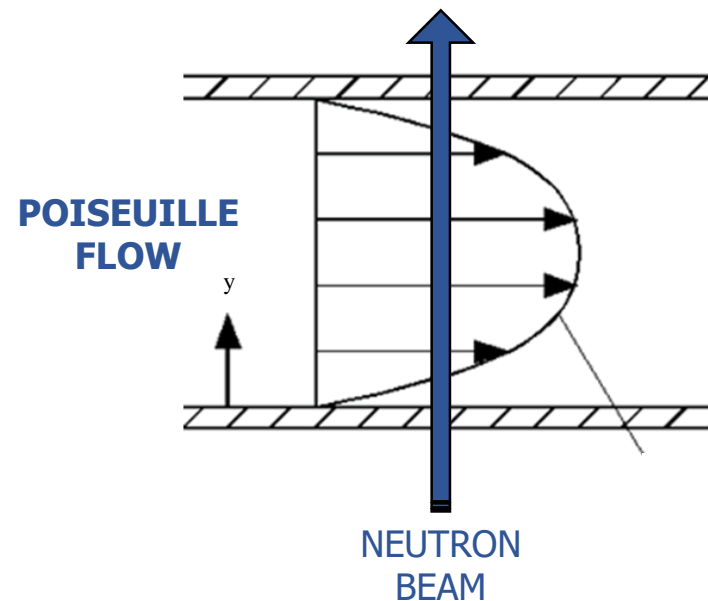


Couette vs Poiseuille RheoSANS

$$\frac{d}{dy}(\text{velocity}) = \dot{\gamma} = \text{constant}$$



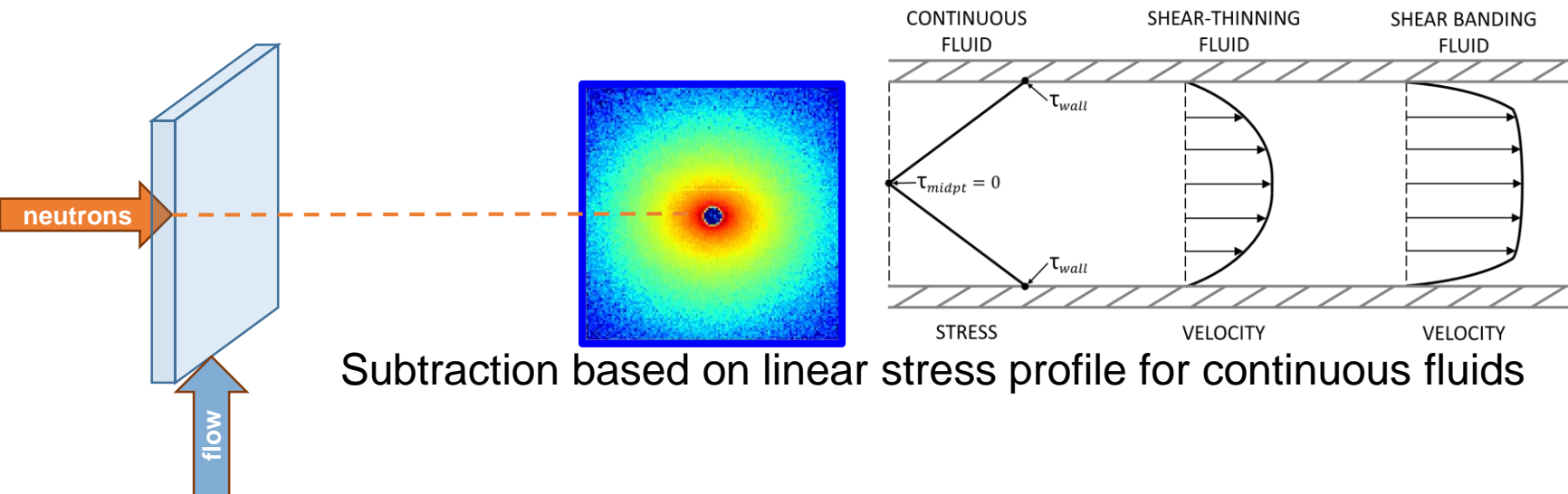
$$\frac{d}{dy}(\text{velocity}) = \dot{\gamma} = f(y, \Delta P, h, w, \eta, \dots)$$



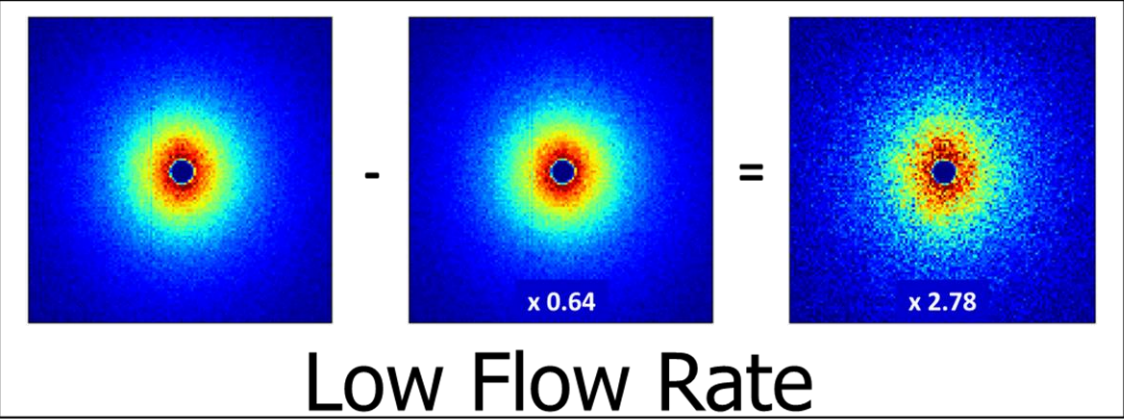
How can we deconvolute the scattering patterns resulting from Poiseuille Flow RheoSANS?

High shear SANS in rectangular channels

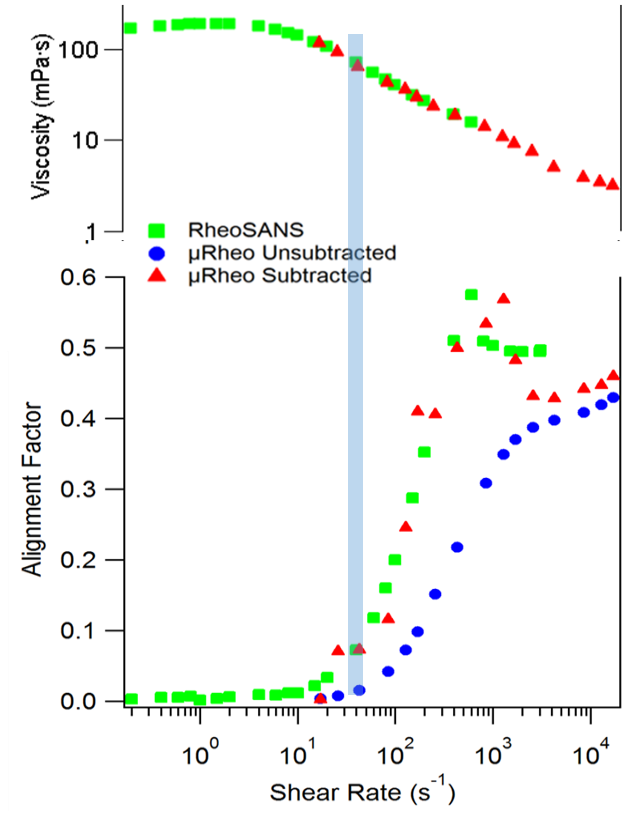
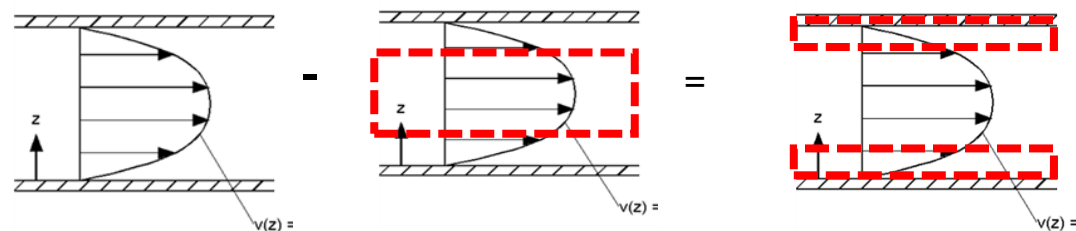
- How to isolate a certain stress, when a whole spectrum is present?
 - Depth sectioning method demonstrated by Fernandez-Ballester et al., JoR '09 (WAXS).
 - Linear stress profile from channel wall to center (continuum)
 - Scattering produced from a superposition of these stress states.
- When the pressure is increased from one state to another, the difference comes only from the highest stress near the channel walls.



Analysis: Determining Structure near the Wall

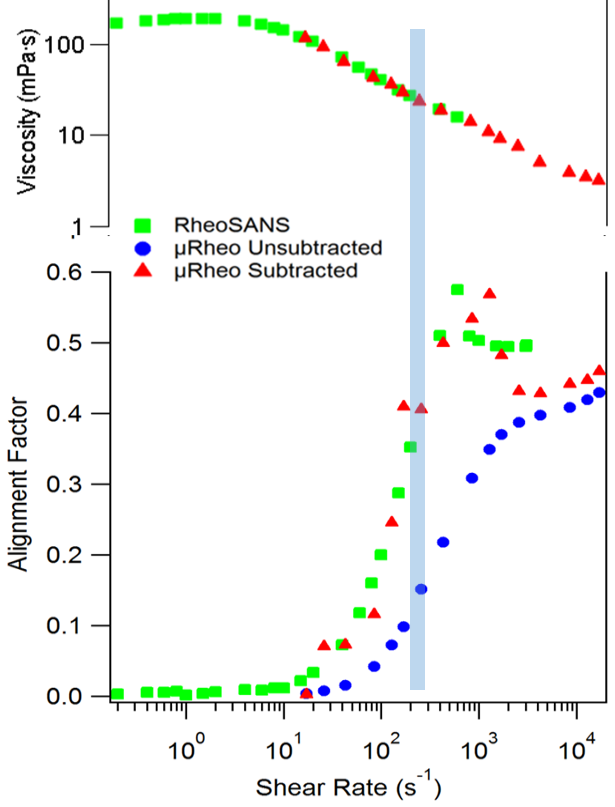
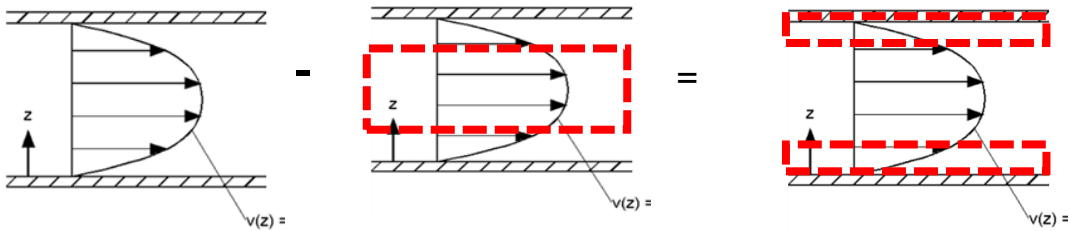
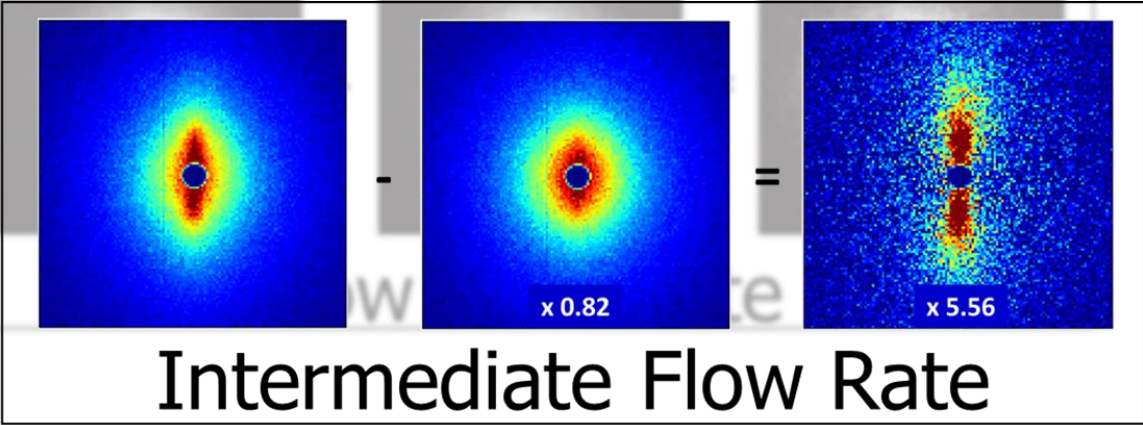


$I(q)$ from entire flow - $I(q)$ from a lower wall stress, scaled 64% = $I(q)$ from the top and bottom 18%, and corrected for new scattering volume (x 2.78)

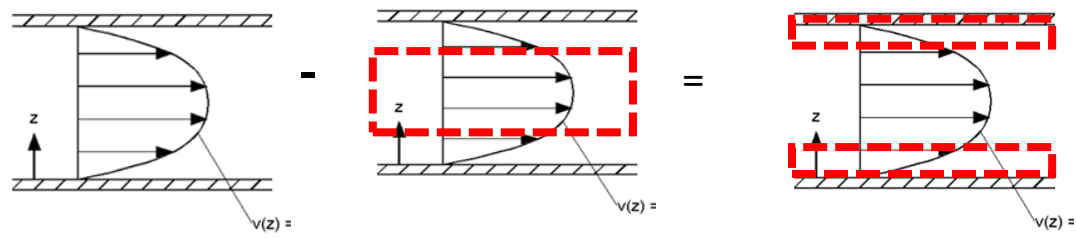
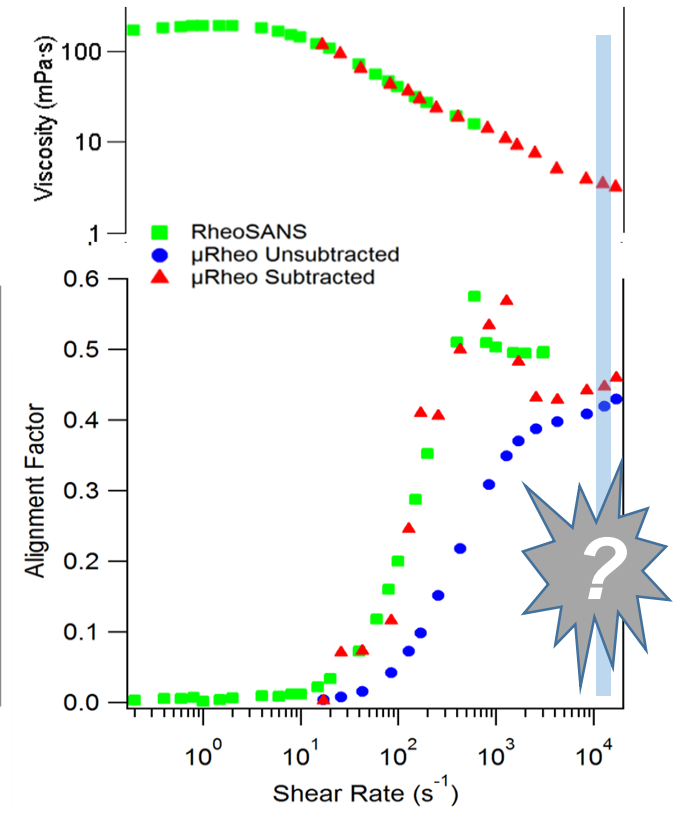
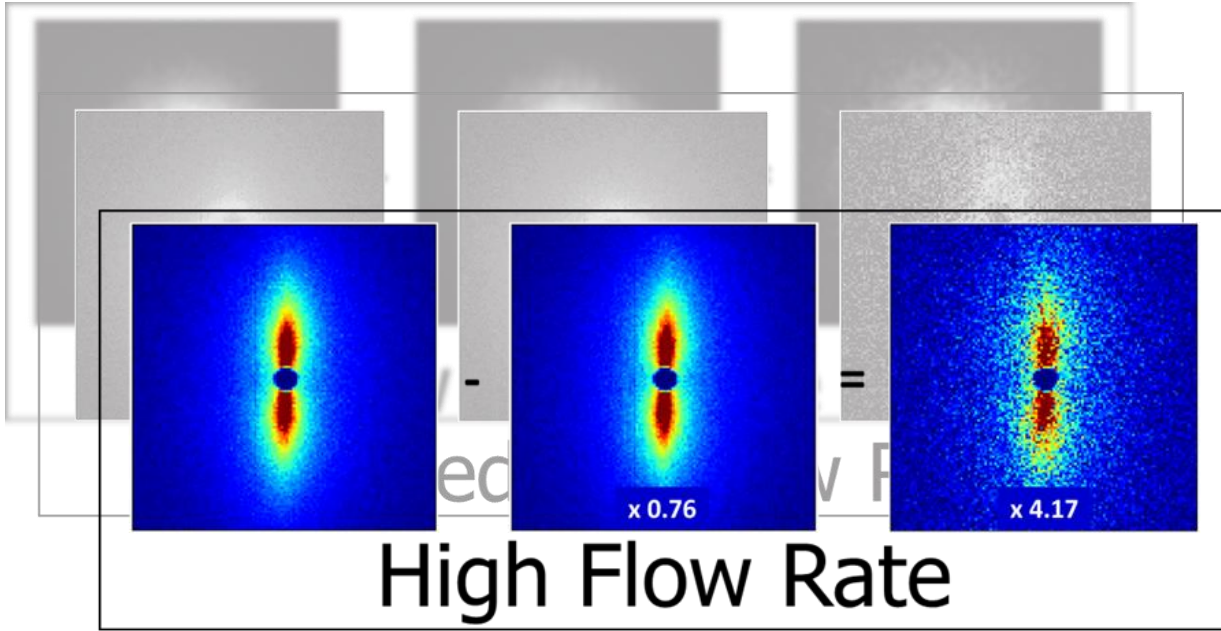


$$I_{q_x, q_y}(wall) = \frac{1}{1 - \frac{\tau_{wall, n-x}}{\tau_{wall, n}}} \left[I_{q_x, q_y}(Q_n) - \frac{\tau_{wall, n-x}}{\tau_{wall, n}} I_{q_x, q_y}(Q_{n-1}) \right]$$

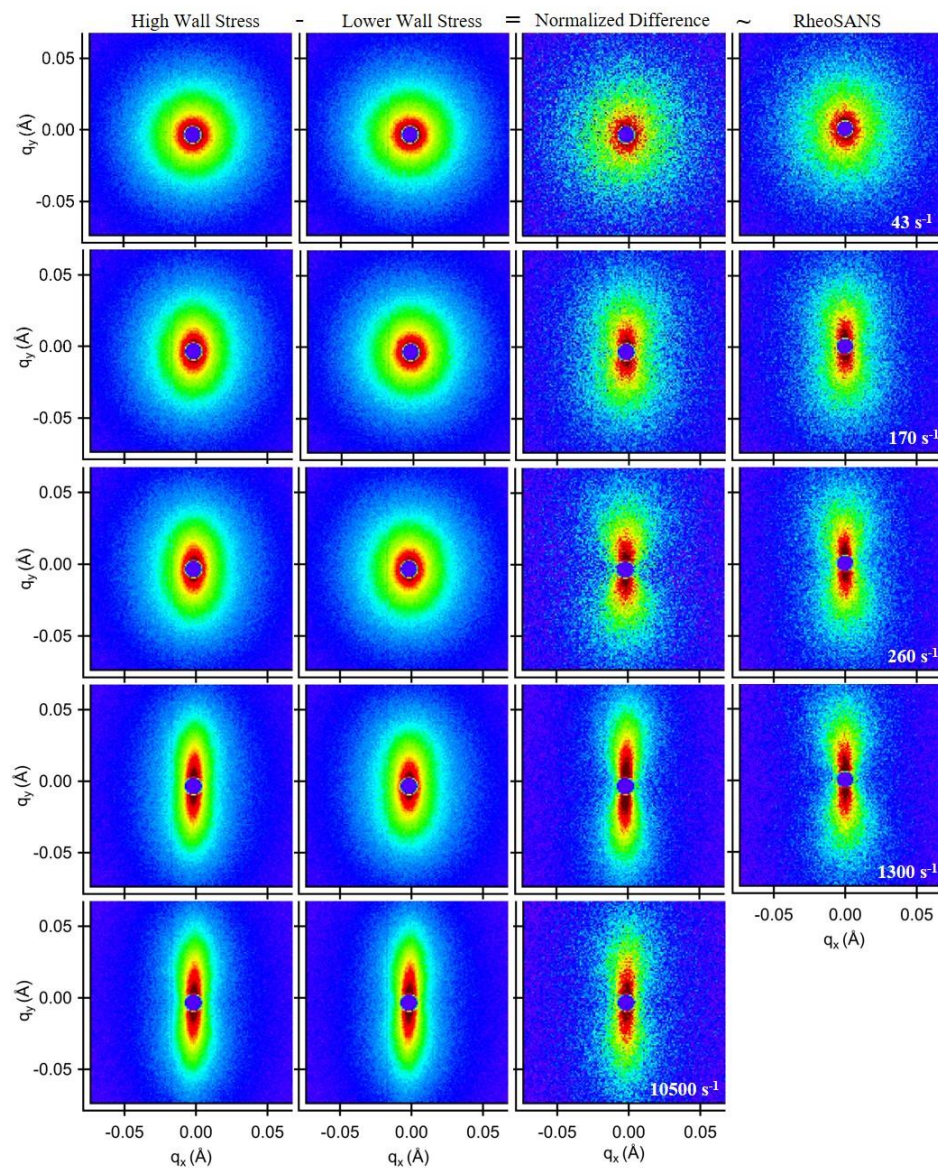
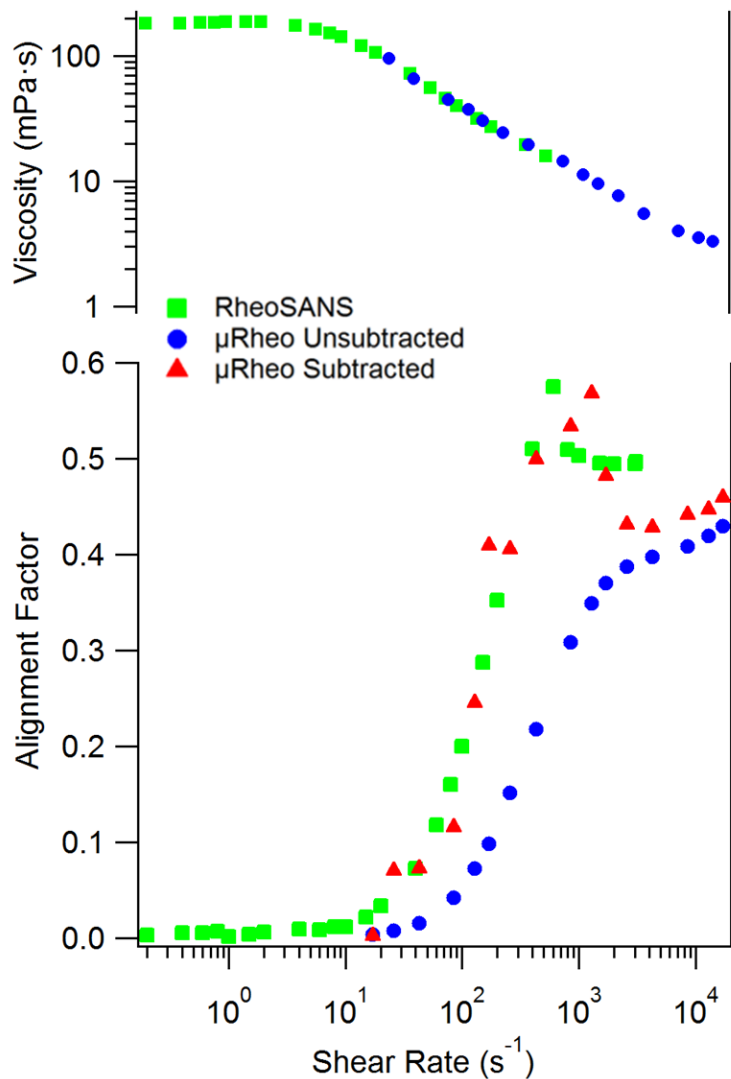
Analysis: Determining Structure near the Wall



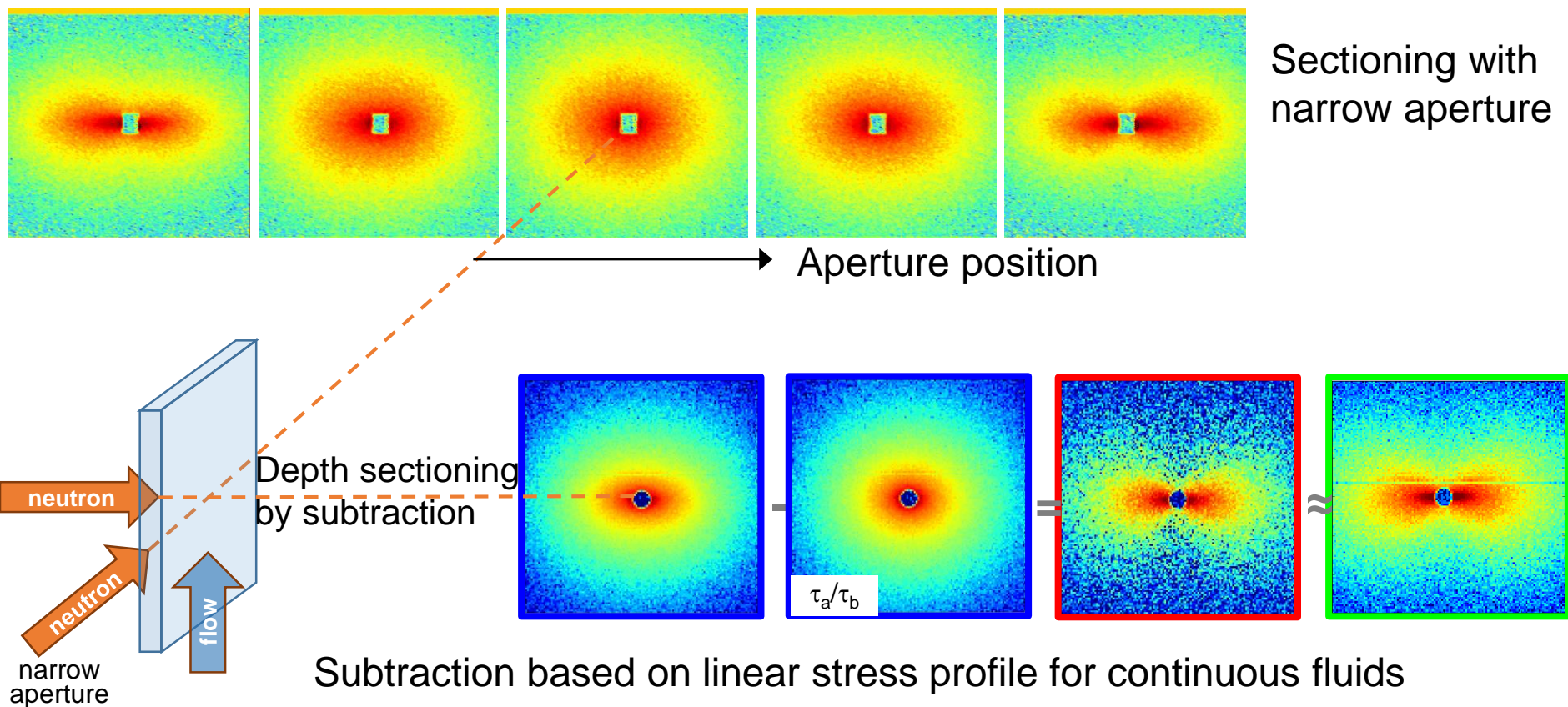
Analysis: Determining Structure near the Wall



μ RheoSANS of Anionic Wormlike Micelles



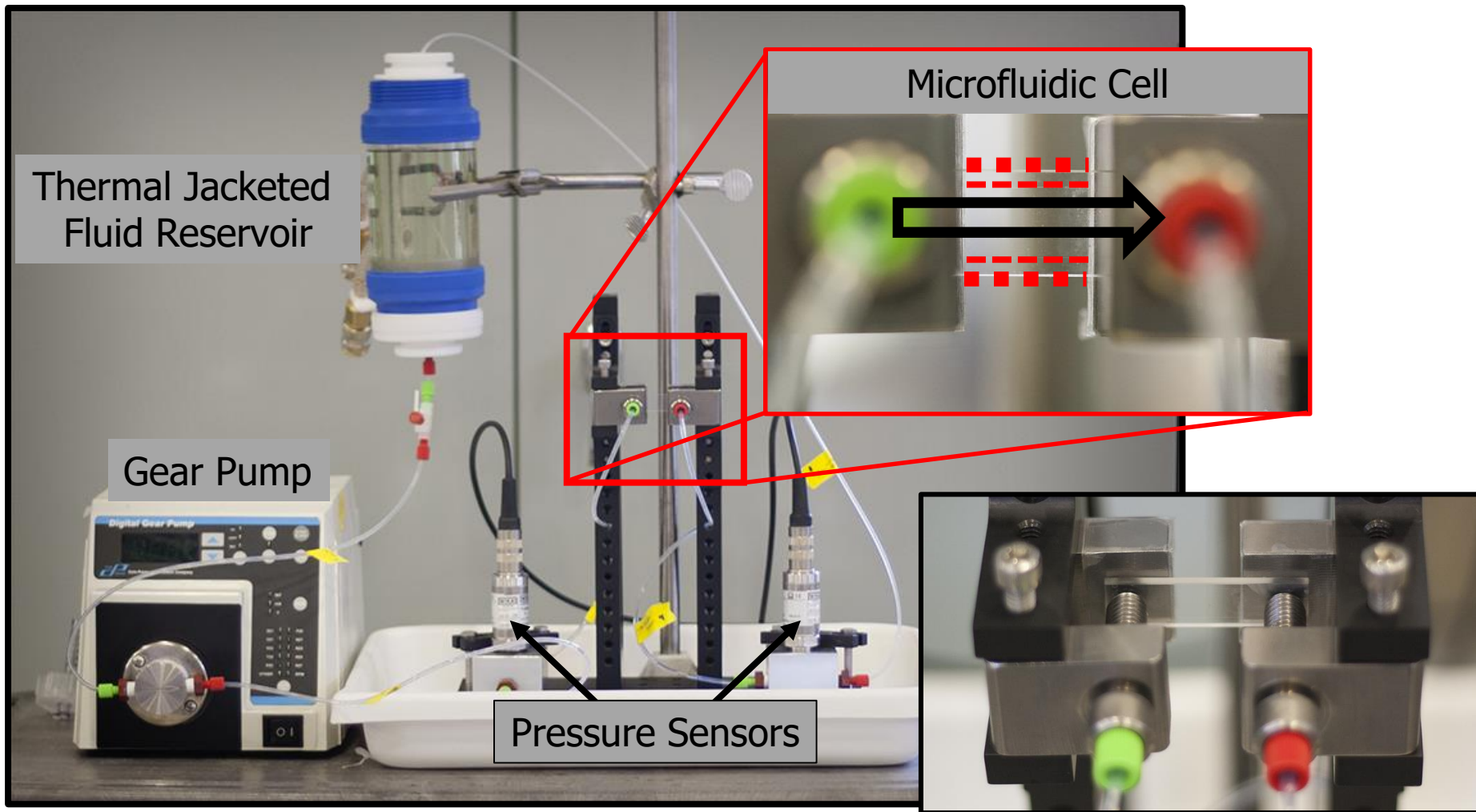
High shear SANS in rectangular channels



μ RheoSANS Limitations

- Depth dependent scattering analysis:
 - Approach will fail if the scattering depends on position independent of stress
 - Concentration gradient
 - Continuous sample (no sample fracture)
 - Slice depth relative to scattering object dimensions
 - Time...
- Pressure drop or flow rate limited in terms of reaching high shear rates...

μ RheoSANS -- Prototype

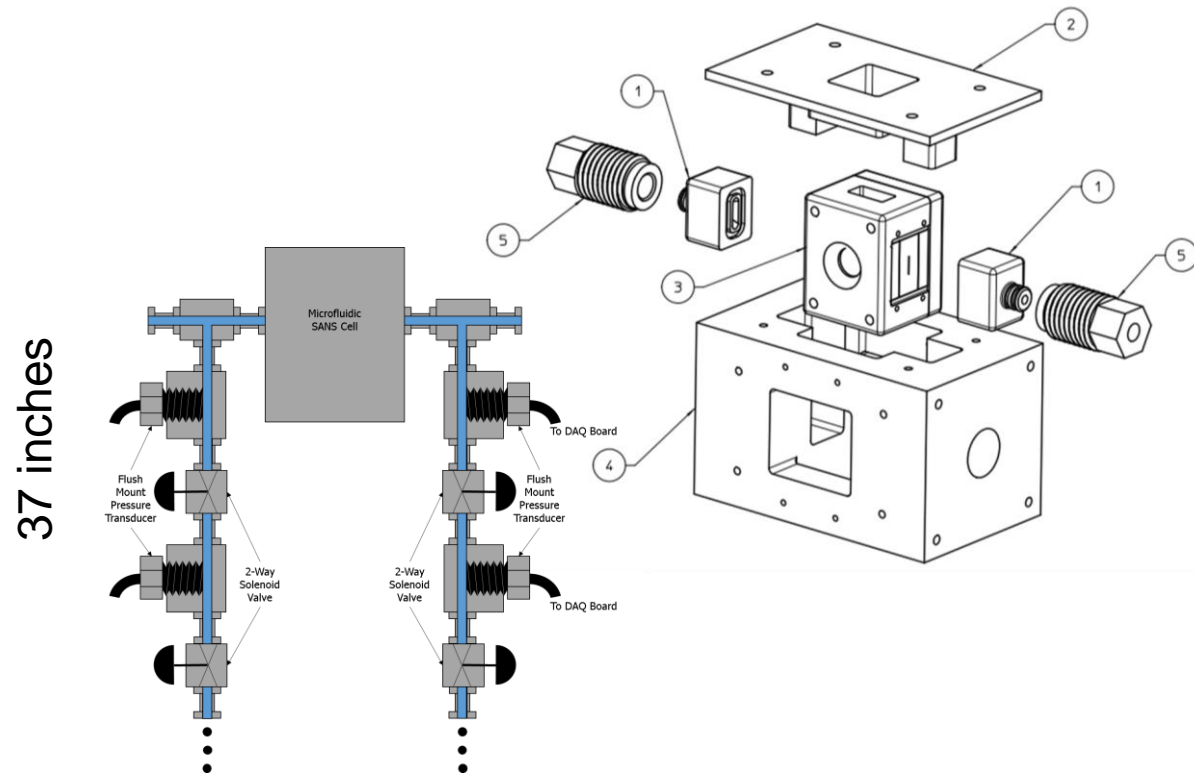
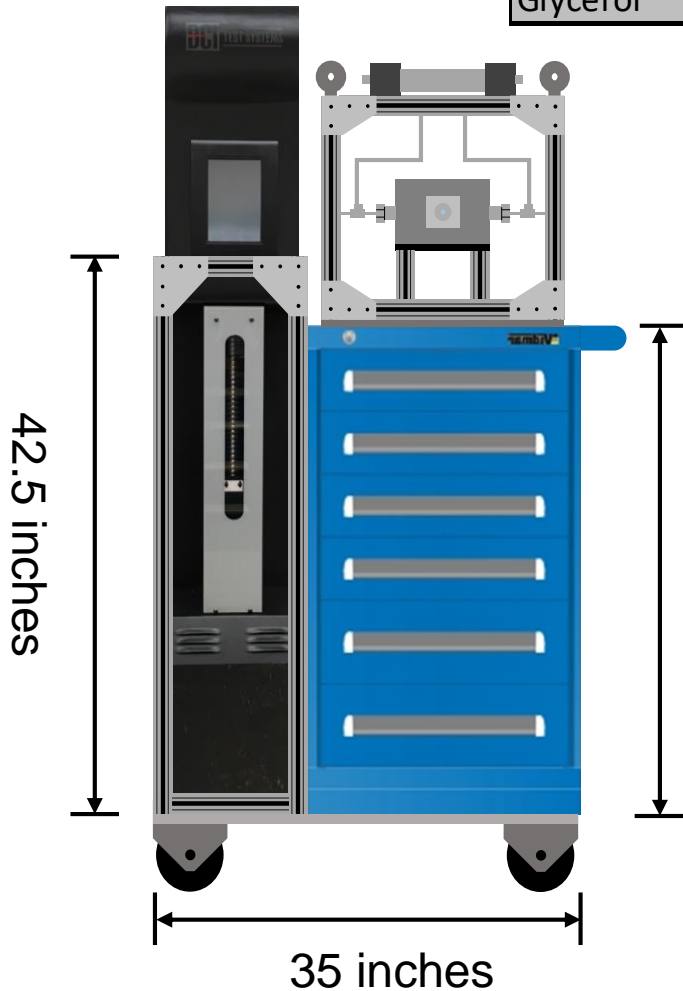


Weston, Seeman, Salipante, Blair, Hudson and Weigandt (In Preparation)

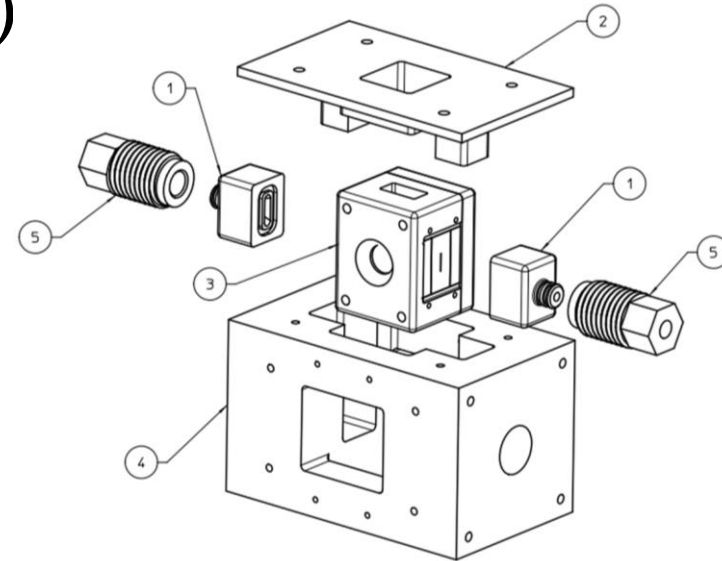
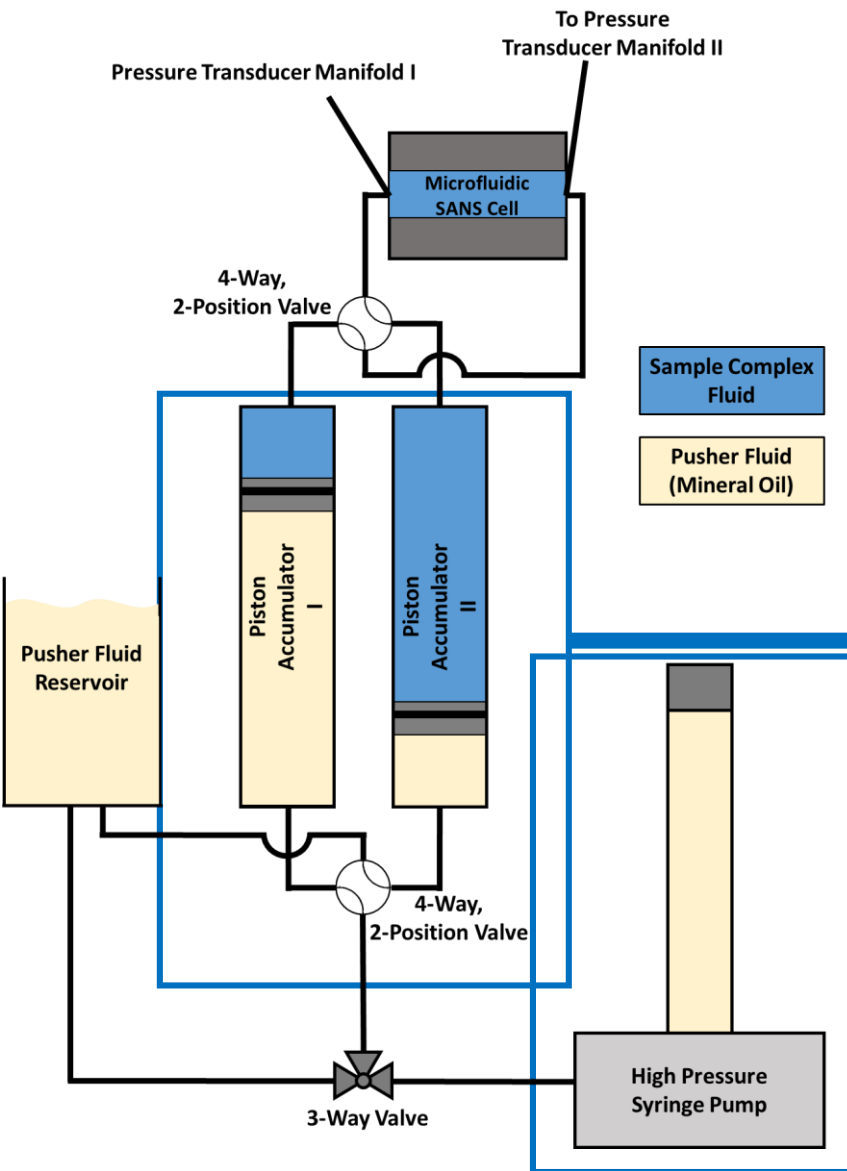
μ RheoSANS Upgrade (high P/SR)

Fluid	Maximum Shear Rate, s^{-1}			Maximum ΔP , psi		
	25 μm	50 μm	100 μm	25 μm	50 μm	100 μm
Water	4.25×10^6	1.07×10^6	2.67×10^5	3500	450	60
Ethylene Glycol	3.08×10^6	1.07×10^6	2.67×10^5	5000	5000	1083
Glycerol	4.10×10^4	8.21×10^4	1.65×10^5	5000	5000	5000

*based on a rectangular channel 15 mm wide x 70 mm long



μ RheoSANS Upgrade (high P/SR)



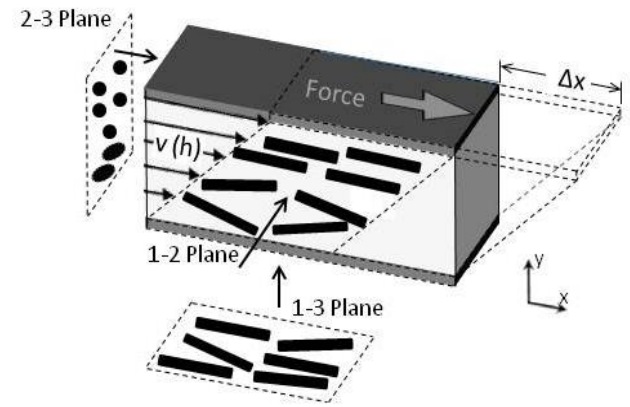
HiP Tubular Reactor w/Piston

- 125 mL each
- 10 000 psi – 700 bar
- 304 Stainless Steel
- 0 – 125°C

DCI VPA Syringe Pump

- 400 mL/min
- 5000 psi – 345 bar
- Stainless Steel Cylinder
- 12 nL volume resolution

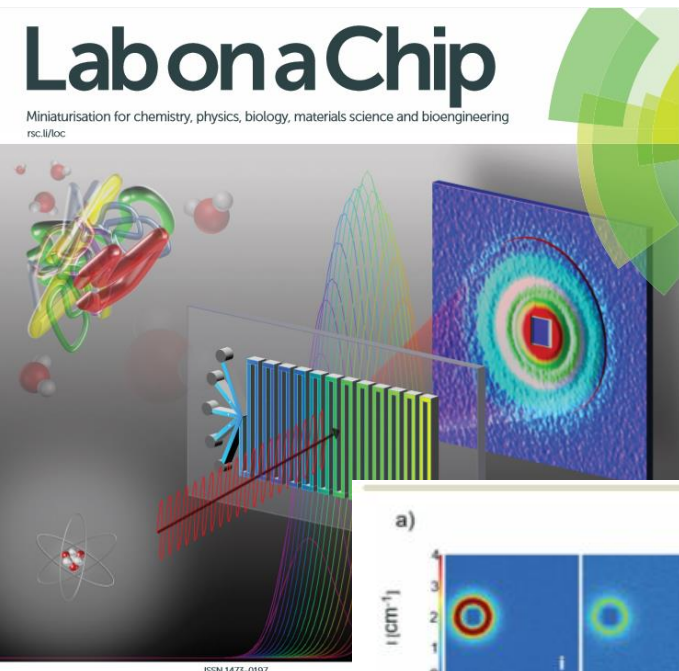
Challenges



- Analysis: Can we get more from our anisotropic 2D data?
Simultaneous fits of data through multiple flow planes?
- Limitations: Communicating limitations without stifling creativity?
- Portability: How easy is it to port new sample environment from one facility to the next?

Extra Slides

Microfluidics-SANS

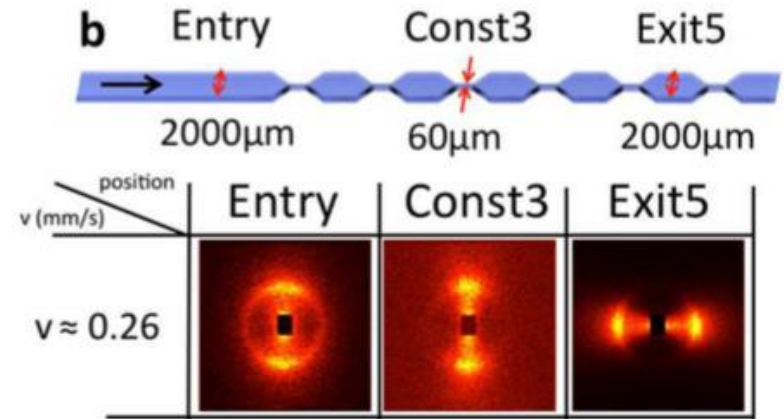
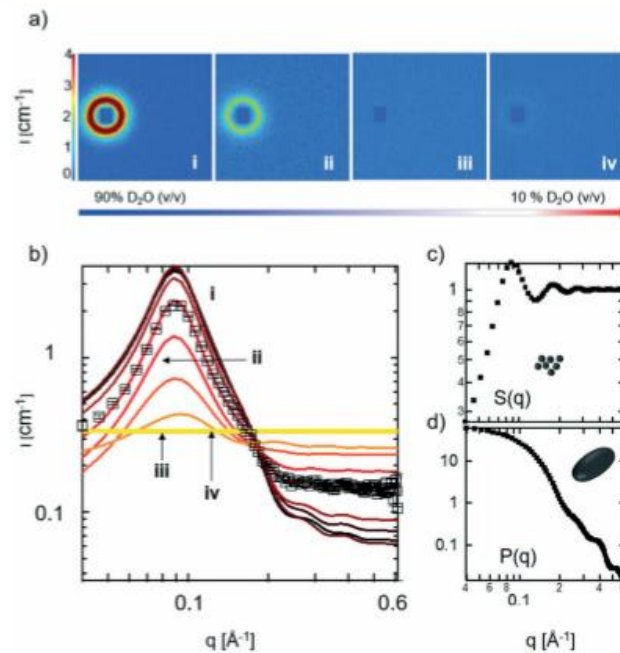


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 Rapid contrast matching by microfluidics

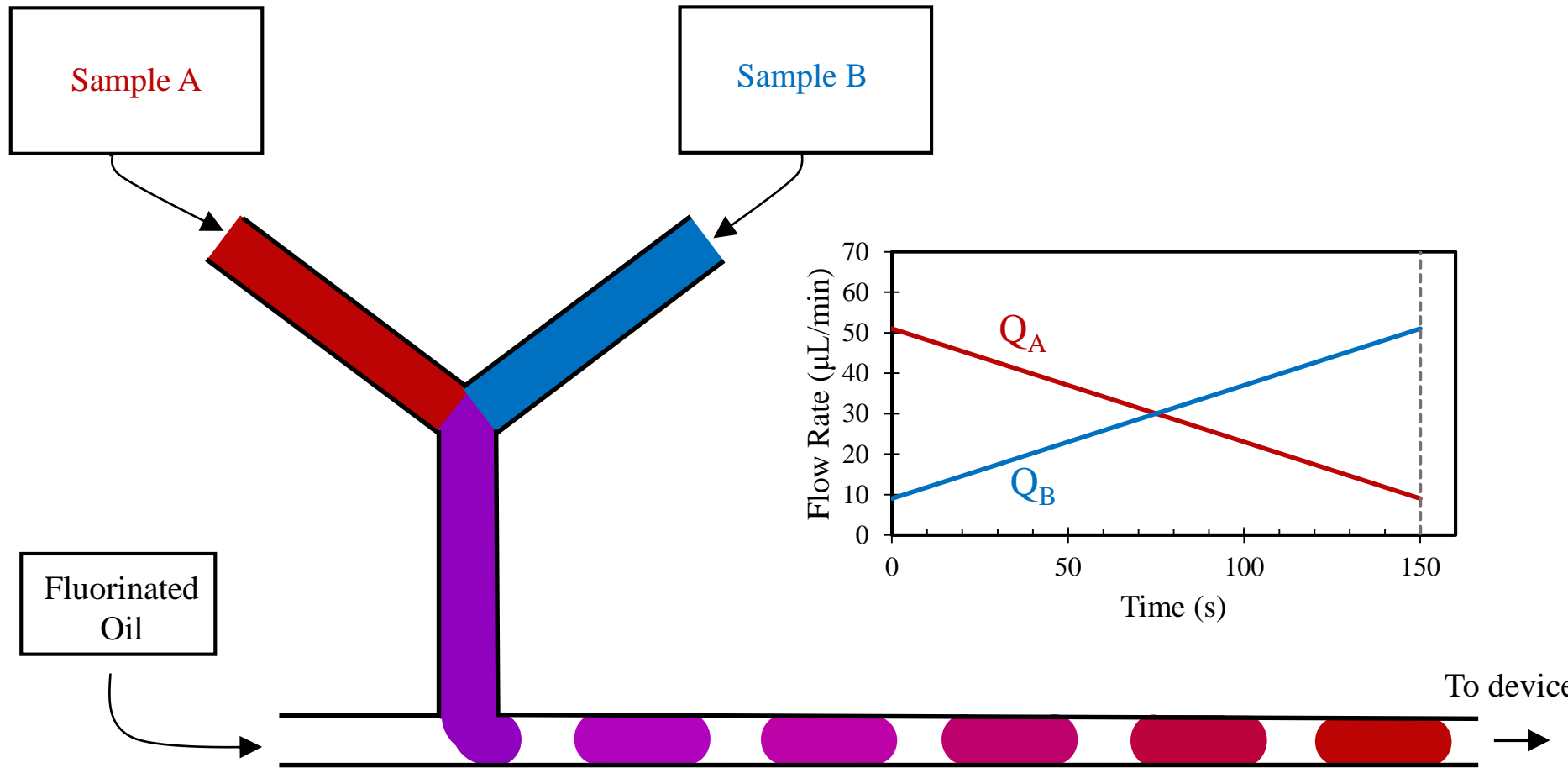
Microfluidic-SANS: flow processing of complex fluids

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Millifluidic SANS -- SANSdrop



- Vary individual syringe pumps to produce concentration gradient
- Keep combined dispersed phase flow rate constant